

A Case Study on Irregularities Present in Tall Building and Review of Provisions on Indian Standard

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Abstract

Irregularities are mainly categorized under the plan and vertical irregularity in IS 1893 (Part 1): 2016 along with precautions for design and analysis in case of occurrence of irregularities. In this paper, an effort is done to identify irregularities present in existing commercial cum residential building satisfying provisions of Indian Standard code, and the complications on the adaption of mitigating measures. It is concluded that re-entrant corner irregularity is rampant in residential apartments and a soft storey is likely with open parking floors and building with variation in storey heights. Also, the three-dimensional vertical analysis method is ambiguous to adopt and the use of equivalent diagonal strut is ineffective with current clauses. Furthermore, additional clarification of weak storey is requisite.

Keywords: Irregularity, re-entrant corners, soft storey, weak storey.

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INTRODUCTION

Irregularity in mass or stiffness in plan and elevation makes a building more vulnerable in case of stability and lateral load resistance. Irregularity hinders uniformity of load path which may cause severe damage in the irregular building than a regular building. So efforts should be done to eliminate irregular configuration by modifying architectural planning. But sometimes irregularities are inevitable so IS 1893(Part 1) has defined types of them with criteria for consideration and some remedial measures are included in 2016 revisions [2]. Irregularities are categorized under Plan and Vertical irregularity. Torsion, Re-entrant corner, Diaphragm Discontinuity, Out-of-Plane Offsets, and Non-Parallel systems are five types of plan irregularities. Additionally, Stiffness, Mass, Vertical Geometric, In-Plane Discontinuity in Vertical Elements Resisting Lateral Force, and Strength Irregularity are defined under Vertical Irregularity in 2002 revision of IS 1893 (Part 1) [1]. Whereas two more kinds of irregularities namely Floating or Stub Columns and Irregular modes of Oscillation in Two Principal Plan Directions are added under Vertical Irregularity in 2016 revision and Diaphragm discontinuity is defined as Floor slabs having excessive cut-outs or opening.

Condition for the existence of some irregularities is revised mainly for Torsional Irregularity, Stiffness, Mass, Strength, Vertical

Geometric, and In-Plane discontinuity. An irregularity check is performed for both the conditions mentioned as per the 2002 and 2016 revision.

Results from the equivalent static method are not appropriate in comparison to the response spectrum method as it doesn't consider irregularity effects and depends only on the empirical formula [3]. Buildings with complex shape should be designed duly taking care of their dynamic behavior [4]. Shorter structures with increased first storey height and taller structures with increased middle storey height generally produce greater inter-storey drift demands than regular storey [5]. Irregularities influences the height wise variation of story drifts with the effect of strength being larger than stiffness [6]. A requirement of Dynamic analysis for irregular buildings as per UBC is validated as Static analysis underestimates the column demands [7]. Distributions of total story shears were reproduced slightly more accurately by the dynamic methods than by the static methods [8].

Building Configuration

An existing seventeen storey multipurpose Tall building (2 Parking + 2 Commercial +13 Residential) was considered to study the irregularities that may present in the building and to analyze provisions of the code on addressing those irregularities. Irregularities checks were performed as per both the revisions of IS 1893 (Part 1) and discussions are done based on the

procedures of quantification of irregularity, measures to be taken, and the discrepancies present in the code.

One of the parking floors was maintained at 3.96m so that it would be easy for parking and all the other floors are 3.05m. Residential floors are planned to maintain proper ventilation and lighting inside the room. Beam layouts of commercial and parking floors are identical whereas changed for residential floors. Dead loads and live loads on each floor are considered as per as per IS 875 (Part 1) and IS 875 (Part 2). The building was analyzed for earthquake loads for the load combinations as per IS 456: 2000. Beam layouts of commercial parking and residential floors are as shown in Fig 1 and 2. And the three dimensional rendered view of the building is shown in Fig-3.

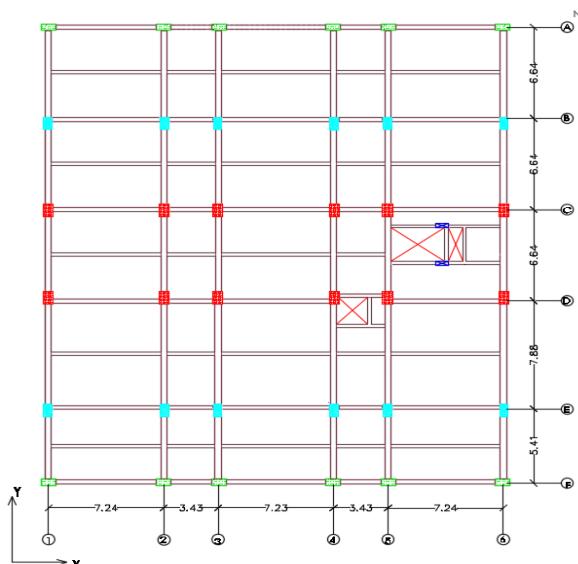


Fig-1: Beam layout of Commercial and Parking floor

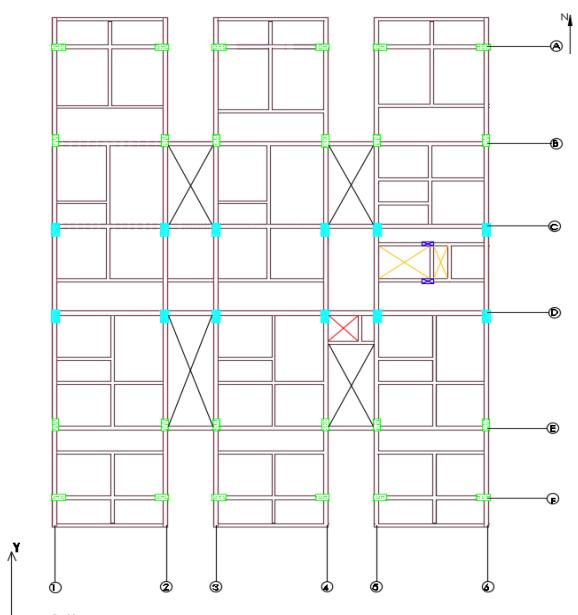


Fig-2: Beam layout of Residential floor

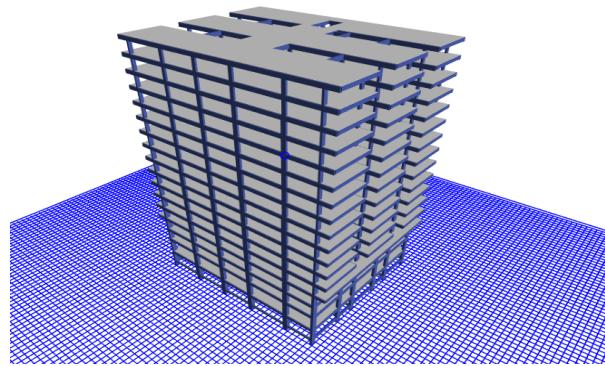


Fig-3: Model in ETABS

Irregularity Check

Irregularity in the building causes the non-uniform distribution of mass and stiffness in plan and elevation which may cause damage. Irregularities and requirements to cope with them are mentioned in Table 5 and 6 [1, 2]. All the irregularity conditions are checked to identify if any present in the building. Also, irregularity is verified as per IS 1893 (Part 1): 2002.

Plan Irregularity

Torsional Irregularity

For displacement

Irregularity is said to exist if the displacement of one end of the floor is 1.5 times its minimum horizontal displacement of the far end [2] while the ratio is 1.2 for the same [1].

a. In X-Direction b. In Y-Direction

$$\begin{aligned} x_1 &= 67.7 \text{ mm} \text{ and } x_2 = 66.8 \text{ mm} \text{ and } y_1 = 58.6 \text{ mm} \text{ and } y_2 = 59.8 \text{ mm} \\ \text{Ratio } (x_1 / x_2)^2 &= 1.01 < 1.5^2 \text{ ratio } (y_2 / y_1)^2 = 1.02 < 1.5^2 \\ &= 1.01 < 1.2^2 = 1.02 < 1.2^2 \end{aligned}$$

For Natural Period

Irregularity exists if the time period of fundamental torsional mode is greater than that of the first two translational modes [2]. The time period for the respective fundamental modes is given in Table-1.

Table-1: Modes with the respective time period

Mode	Period (sec)
1 (Translation)	2.332
2 (Translational)	2.285
3 (Torsional)	2.095

Natural period in fundamental torsional mode = 2.095 sec < 2.332 sec,
= 2.095 sec < 2.285 sec

As both the requirements are not satisfied Torsional irregularity is not present in the building

Re-entrant Corners

The re-entrant corner is said to exist if a projection of size greater than 15 % of its overall plan dimension in that direction [1, 2].

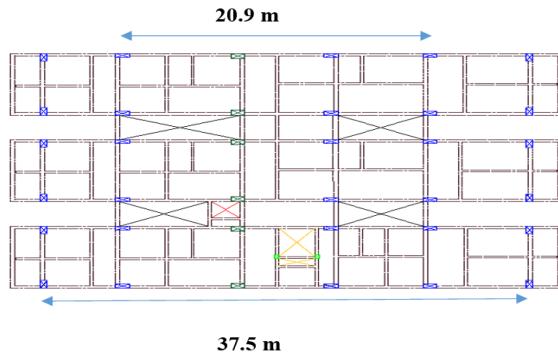


Fig-4: Beam layout of building with dimension for a re-entrant corner

From Fig-4 projection of 20.9m is observed for a span of 37.5m.

So, Projection percentage = $(20.9/37.5) * 100 = 55.7\% > 15\%$

Re-entrant corner exists in building hence three-dimensional dynamic analysis shall be adopted.

Floor slabs having excessive Cut-outs or Opening

No such openings are present in the building considered.

Out-Of-Plane Offsets in Vertical Elements

Offsets in vertical Elements are not present in building Considered.

Non-Parallel Lateral Force System

Irregularity is said to exist if all the structural systems resisting lateral forces are not oriented along two principal orthogonal axes in the plan. As shown in Fig-5. All the lateral load resisting elements i.e. Columns are oriented in two principal orthogonal directions in the building considered as shown in Fig-6. So the irregularity is not present in the building considered.

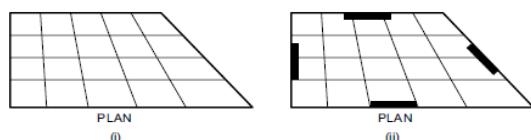


Fig-5: Non-Parallel lateral force system

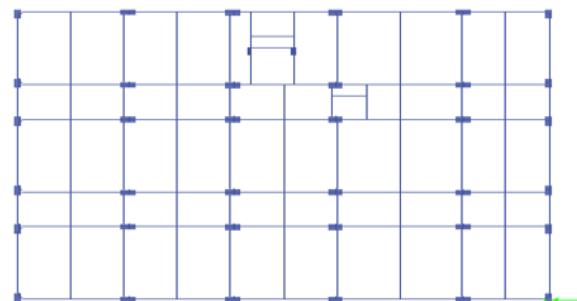


Fig-6: Layout with Lateral force system.

Vertical Irregularity

Stiffness irregularity (Soft Storey)

The soft storey is said to exist if lateral stiffness of any storey is less than that of the storey above i.e. $K_{i+1} > k_i$ [2] while the soft storey was defined to be the storey which lateral stiffness is less than 70% of the above storey or 80percent of the average lateral stiffness of three storeys above in previous revision [1].

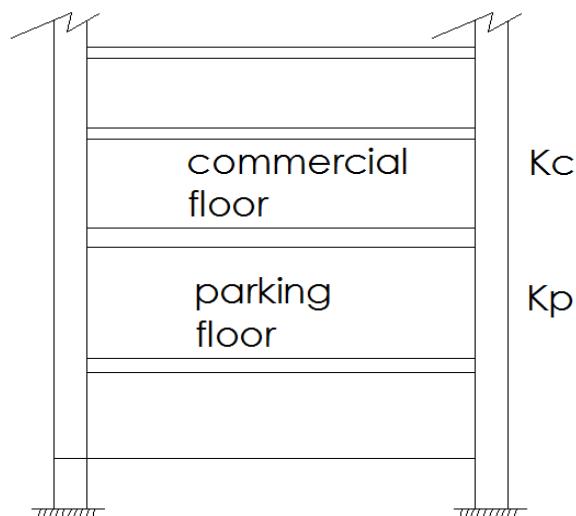


Fig-7: Section of elevation indicating different types of floors

Table-2: Lateral Stiffness calculation of Parking Floor

Column Sizes (mm)	No.	I _{xx} (mm ⁴)	I _{yy} (mm ⁴)	E (N/mm ²)	H (mm)	K _x (N/mm)	K _y (N/mm)
910 x 460	6	173321330000	44287880000	27386	3960	917230	234375
910 x 530	6	67739035000	199696315000	27386	3960	358480	1056809
910 x 610	6	103276355000	229839155000	27386	3960	546547	1216327
910 x 610	6	103276355000	229839155000	27386	3960	546547	1216327
910 x 530	6	67739035000	199696315000	27386	3960	358480	1056809
910 x 460	6	173321330000	44287880000	27386	3960	917230	234375
					Total	3644515	5015022

Table-3: Lateral Stiffness calculation of Commercial Floor

Column Sizes (mm)	No.	I _{xx} (mm ⁴)	I _{yy} (mm ⁴)	E (N/mm ²)	H (mm)	K _x (N/mm)	K _y (N/mm)
910 x 460	6	173321330000	44287880000	27386	3050	2007541	512976
910 x 530	6	67739035000	199696315000	27386	3050	784606	2313036
910 x 610	6	103276355000	229839155000	27386	3050	1196226	2662174
910 x 610	6	103276355000	229839155000	27386	3050	1196226	2662174
910 x 530	6	67739035000	199696315000	27386	3050	784606	2313036
910 x 460	6	173321330000	44287880000	27386	3050	2007541	512976
					Total	7976745	10976373

Table-4: Error! No text of specified style in document. Lateral Stiffness calculation of Residential Floor

Column Sizes (mm)	No.	I _{xx} (mm ⁴)	I _{yy} (mm ⁴)	E (N/mm ²)	H (mm)	K _x (N/mm)	K _y (N/mm)
910 x 460	6	173321330000	44287880000	27386	3050	2007541	512976
910 x 460	6	44287880000	173321330000	27386	3050	512976	2007541
910 x 530	6	67739035000	199696315000	27386	3050	784606	2313036
910 x 530	6	67739035000	199696315000	27386	3050	784606	2313036
910 x 460	6	44287880000	173321330000	27386	3050	512976	2007541
910 x 460	6	173321330000	44287880000	27386	3050	2007541	512976
					Total	6610246	9667107

Stiffness irregularity is checked for three different floor levels as shown in Fig-7 for which lateral stiffness is calculated as shown in Tables 2, 3 and 4 for parking, commercial and residential floor respectively. Lateral stiffness of parking floor (K_p) with height 3.96m $K_p = 3644514.5 \text{ kN/m}$

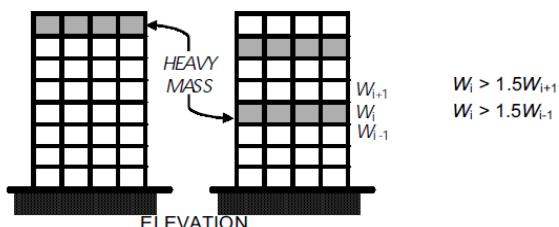
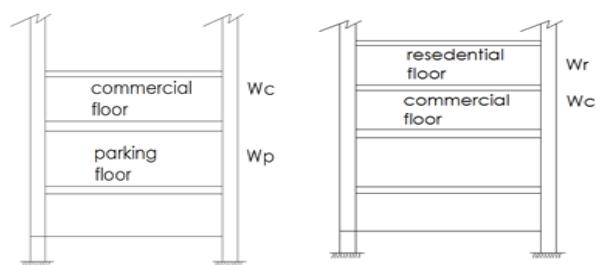
Lateral Stiffness of commercial floor (K_c) with height 3.05 m $K_c = 7976745.3 \text{ kN/m}$ Lateral Stiffness of Residential floor (K_r) with height 3.05 m $K_r = 6610245.6 \text{ kN/m}$

Lateral Stiffness of commercial floor $K_c > K_p$ Lateral stiffness of parking floor. Also $(K_p / K_c) \times 100 = 45\% < 70\%$

So there is stiffness irregularity between Parking and commercial floor as per both revisions. But $K_r < K_c$ so Stiffness irregularity does not exist between commercial and residential floor.

Mass Irregularity

Mass irregularity shall be considered to exist when the seismic weight of any floor is more than 150 % [2] and 200% [1] of that of the floors below respectively as shown in Fig-8.

**Fig-8: Indication for Mass Irregularity****Fig-9: Section of elevation indicating different types of floors**

Seismic weight is calculated for three different floors as shown in Fig-9 whose loads are different from one another and compared for the presence of mass irregularity.

Seismic weight of the commercial floor $W_c = 10951.7 \text{ kN}$ and

Seismic weight of the parking floor $W_p = 10669.5 \text{ kN}$ Percentage seismic weight of commercial floor = $102.6\% < 150\% < 200\%$.

So mass irregularity is not present between the commercial and parking floor.

The seismic weight of the commercial floor $W_c = 10951.7 \text{ kN}$

Seismic weight of residential floor $W_r = 13026.8 \text{ kN}$ Percentage seismic weight of residential floor = $118.9\% < 150\% < 200\%$.

So mass irregularity is not present between the commercial and residential floor.

Vertical Geometric Irregularity

Irregularity is said to exist if the Horizontal Dimension of lateral load force-resisting system in any

storey is more than 125% and 150% of the storey below [2, 1]. No such projection is present in building considered.

In-Plane Discontinuity in Vertical Elements Resisting Lateral Force

Irregularity exists if In-Plane offset of the lateral force-resisting elements is greater than 20% of the plan length of that element [2] while 2002 revision has not fixed the percentage [1]. No such offset in lateral force resisting element is present in the building considered.

Strength Irregularity (Weak Storey)

The storey weak in stiffness can also be considered weak in strength thus strength irregularity exists in the building. As the lateral load resisting

members are the same in the floors there seems no distinct way defines by the standard to determine the strength.

Floating or Stub Column

Such columns are not present in the building considered.

Irregular Modes of Oscillation in Two Principal Plan Direction

Irregularity of Irregular modes of Oscillation is newly mentioned provision in latest revision [2].

- First three modes contribute less than 65% mass participation factor in each principal plane. Mass participation for all three fundamental modes is presented in Table 5.

Table-5: Mass participation in Different modes

No of Mode	Mass participation factor in x	Mass participation factor in y
1	0.801	4.165E-06
2	4.469E-06	0.8437
3	9.144E-06	0.0038

Mass Participation factor in both orthogonal directions is 80.1% in X and 84.4% in Y > 65%.

b. fundamental lateral natural periods of the building in the two principal plan directions are closer to each other by 10 % of the larger value.

apartment buildings as discontinuities are must for lighting and ventilation purposes i.e. for windows

Remedial Measures

The 20162 revision of IS 1893 (Part 1) has mentioned the methods to deal with irregularities and their limitations.

Vertical Earthquake Effects

Consideration of vertical ground shaking has been suggested in Cl. 6.3.3.1 for structures located in Zone IV or V and also if the structure has vertical or plan irregularity along with other requisites. Though the load combinations and considerations of the amount of load factor are specified together with design seismic acceleration spectral value Av the adoption of vertical shaking in the conditions specified seems vague. So, code provisions should clarify the procedures for the application of vertical earthquake effect for unavoidable.

Re-Entrant Corner

Irregularity in plan mostly in residential apartment buildings is present for ventilation and lighting as shown in the above inspection of irregularity in the considered building. Three-dimensional dynamic analysis is recommended to cope with a re-entrant corner in 2016 revision in addition to the Cl. 6.3.3.1 about vertical earthquake effects and Cl 7.7.1 requirement of linear dynamic analysis for any irregular building. Which leaves a query that is it a necessity for vertical earthquake and dynamic analysis for apartment buildings of height around 15m also because the re-entrant corner appears to be unavoidable.

Table-6: Modes with the respective time period

No of Mode	Period (sec)
1	2.332
2	2.285

From Table-6 the percentage of difference in natural periods of fundamental modes is equal to:
 $= (2.332-2.285)/2.332 *100$
 $= 2.02\% << 10 \%$

As both, the requirement does not satisfy the irregularity is absent in the building considered.

Irregularities mentioned in Table 5 and 6 as per Cl. 7.1 are checked and namely Re-entrant Corner in plan and Stiffness Irregularity among Vertical Irregularities are present in the tall building considered. The re-entrant corner is present in all residential floors and vertical irregularity was present in the parking floor with a height of 3.96m.

DISCUSSIONS ON CODE PROVISIONS

Irregularities some times are inevitable like stiffness irregularity and Re-entrant corner as shown above in general or regular practiced buildings. The soft storey is susceptible when storey height is raised for parking or seminar hall and sometimes for movie theatre in commercial buildings. Likewise, Re-entrant corner irregularity seems widespread in residential

Vertical Irregularity (Soft Storey)

- The soft storey is caused mainly due to increased storey height or open storey. Both 20021 and 20162 revisions have recommended some measures as
- Placement of RC structural wall with proper foundation and connection with moment resisting frame which is only possible for a soft or open storey in the ground floor or so. But for the case of occurrence of a soft storey in upper floors for seminar halls or movie theatre shear wall is absurd which if provided also causes difficulties for practical implication and certainly will increase stiffness beyond the lower storey which again makes a lower storey a soft storey or should be provided throughout the height of the building which increases the cost of construction.
 - Braced frame in selected bays of the building, which increases the lateral stiffness of the soft storey. In doing so additional torsion may occur because of limited stiffer bays and also stiffness should be checked not to be much larger than a lower storey which in turn creates another soft storey below that floor.
 - Equivalent Diagonal Strut for Unreinforced Masonry Infill Walls in RC Frame.

Other than above-mentioned provisions 20162 revision recommends the estimation of stiffness contribution by Unreinforced Masonry URM infill by the introduction of an Equivalent Diagonal Strut in the analysis to address the additional stiffness and strength provided by infill.

A sample wall section was considered to check for the possibility of an equivalent diagonal strut as per Cl. 7.9 of IS 1893 (Part 1): 2016 as shown in Fig-10.

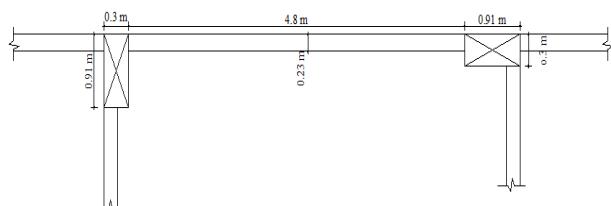


Fig-10: Portion of wall and column arrangement under consideration

Clear length of wall = 4.8m

The thickness of wall = 0.23m

Storey height = 3.05m

Column section = 910mm x 300mm

Beam Section = 300mm x 600mm

Clear height h = 3.05 – 0.6 = 2.45 m

Width of equivalent diagonal strut $w_{ds} = 0.175\alpha_h^{-0.4}L_{ds}$

Where, $\alpha_h = h \left(\sqrt{\frac{E_m t \sin 2\theta}{4E_f I_c h}} \right)$ and Lds = diagonal length

$$I_{C_1} = \frac{920 \times 310^3}{12} = 2.28 \times 10^9 \text{ mm}^4$$

$$I_{C_2} = \frac{310 \times 920^3}{12} = 2.011 \times 10^{10} \text{ mm}^4$$

$$L_{ds} = \sqrt{2.45^2 + 4.84^2} = 5.42 \text{ m}$$

$$\theta = \tan^{-1} \frac{2.45}{4.84} = 26.85^\circ$$

Now, Em= f_m 550

$$f_m = 0.433 f_b^{0.64} f_{mo}^{0.36} =$$

$$0.433 \times 3^{0.64} \times 5^{0.36} = 1.5613$$

$$Em = 550 \times 1.5613 = 858.692 \text{ N/mm}^2$$

$$Ef = 5000 \sqrt{f_{ck}} = 25000 \text{ N/mm}^2$$

$$I_{C_1} = \frac{920 \times 310^3}{12} = 2.28 \times 10^9 \text{ mm}^4$$

$$I_{C_2} = \frac{310 \times 920^3}{12} = 2.011 \times 10^{10} \text{ mm}^4$$

Now solving for $\alpha_h = 1.20$

Width of equivalent diagonal strut

$$w_{ds} = 0.175\alpha_h^{-0.4}L_{ds}$$

$$= 0.175 \times 1.20 - 0.4 \times 5420$$

$$= 881.59 \text{ mm}$$

For the requirements of height to thickness and length to thickness ratios (Cl.7.9.2.2, d)

$$h/t = 2450/228.6 = 10.72 < 12 \dots\dots \text{Ok}$$

$$l/t = 4840/228.6 = 21.17 > 12 \dots\dots \text{not ok}$$

If the thickness of the wall is 115mm

$$h/t = 2450/115 = 21.30 > 12$$

So, to satisfy the conditions of $l/t < 12$

$$1 < 12 \times 115 = 1038 \text{ mm for } 115 \text{ mm wall and}$$

$$1 < 12 \times 230 = 2760 \text{ mm for } 230 \text{ mm wall}$$

Hence the requirement could not be satisfied so Equivalent Diagonal Strut could not be placed in the analysis. Which makes the provision questionable for its purpose if we can't adapt it for more than 3m clear span for 230mm wall and, it is unlikely to consider the use of strut in 115mm wall.

Stiffness and Strength Irregularity

Stiffness is the force needed to cause a unit deflection and can be calculated as the slope of force-displacement whereas strength is a total force that a system can resist. Though both irregularities are differently defined in IS 1893 (Part 1) both seems to be very closely interrelated as the storey with stiffness irregularity likely to be a week in lateral strength too. Furthermore, code has undefined how can we quantify week storey as there is ambiguity on the procedure to calculate lateral strength. So there is a need for clarification about the presence of soft and week storey

whether can exist independently or co-exist in a building.

RESULTS

1. Irregularity of Re-entrant corners is present for lighting and ventilation purpose in apartment buildings regardless of their height.
2. Soft storey present in the building is most likely if the variation of the height of storey is done.
3. Three-dimensional dynamic analysis procedure and consideration required to be more distinctly described.
4. Recommended use of equivalent diagonal strut for unreinforced masonry infill wall cannot be effectively accomplished satisfying the current provision of height to thickness and length to thickness ratios.
5. Strength irregularity and approach of its determination should be further defined along with its occurrence with and without the soft story.

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